



Computing & Microfluidics Lab

國立成功大學工程科學系

計算與微流體晶片實驗室

# Adaptive CESE Method for Solving Unsteady Euler Equations

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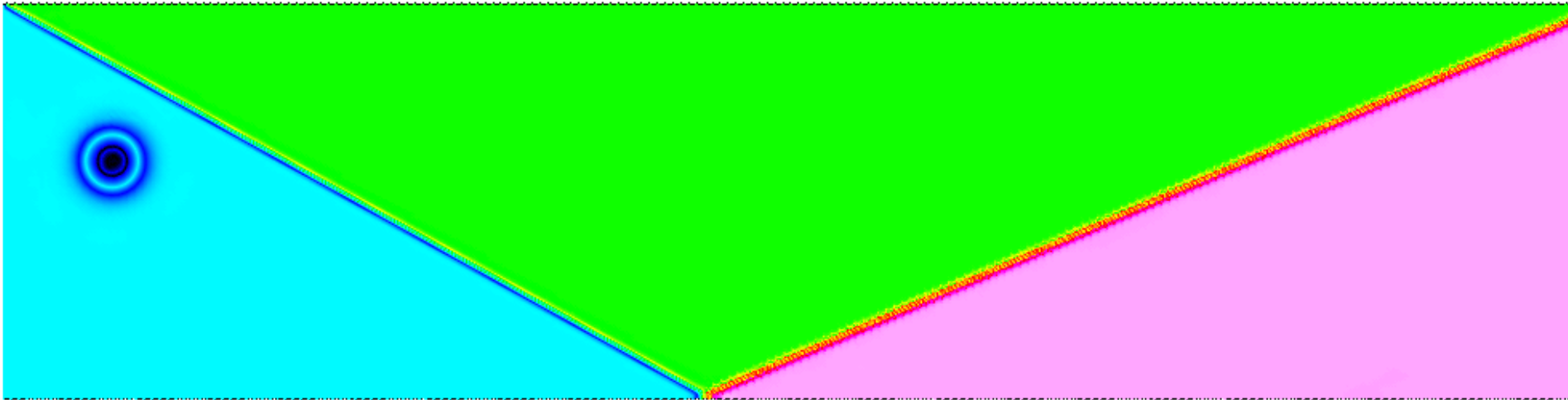


*To Tony Sheu*

**Wishing you**  
**Good spirit, Good health,**  
**Keep random walk with deterministic mind**  
**Enjoy life!**



# *Introduction*



## Shock Vortex Interaction

Flow discontinuities, Unsteady waves,

Accuracy, Easy treatment of BCs, Length Scales

NASA Glenn Research Center website:  
<http://www.grc.nasa.gov/WWW/microbus/>



# *The Inventor of the CESE Method*



Dr. Sin-Chung Chang  
NASA Glenn Research Center

Chang SC, (1995), The method of space-time conservation element and solution element– a new approach for solving the Navier-Stokes and Euler equations, *Journal of Computational Physics*, 119, 295-324.



# *CESE Method*

- (1) The method is a complete explicit scheme.
- (2) Non-dissipative scheme.
- (3) Add numerical dissipation as desired.
- (4) Enforced space-time flux conservation, local/global flux conservation.
- (5) The spatial derivative  $\frac{\partial u}{\partial x}$  is treated as unknown variable w/o discretization.
- (6) No flux reconstruction at mesh interface (Riemann problem).



# *Our Former CESE Applications*

## *Shock Diffraction*



### **Shock Diffraction over a 75 degrees corner ( $M_0=2.5$ ) Density Contours**



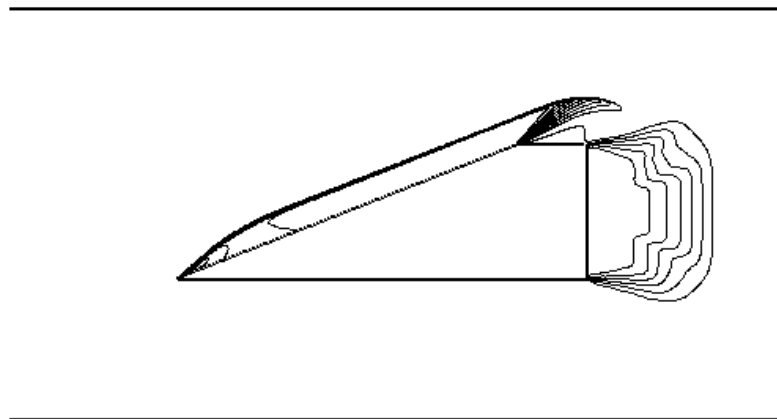
**CE/SE Group  
NCKU ES Computing & Microfluidics Lab.**

Tseng T and Yang RJ 2005, *Shock Waves*, Vol. 14, 307-311



# *Our Former CESE Applications*

## *Supersonic Flow over a Wedge*

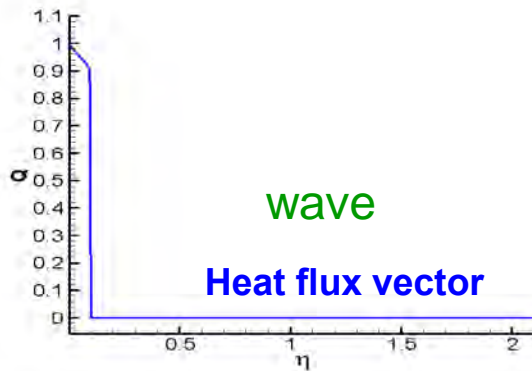
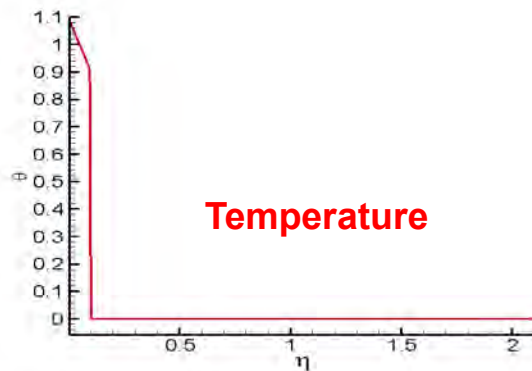


Tseng T and Yang RJ 2006, *AIAA Journal*, Vol.44, 1040-1047

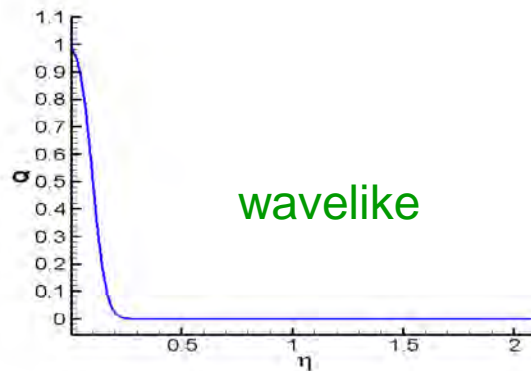
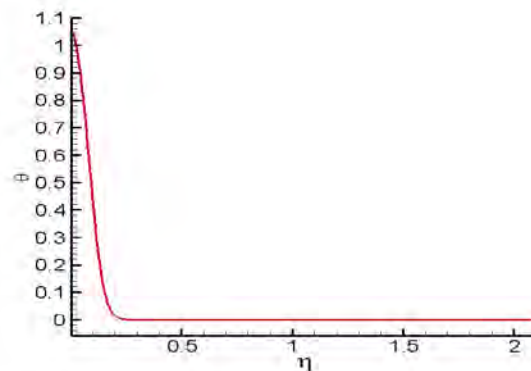
# 1-D Thermal Waves

Presentation of wave, wavelike and diffusion behaviors

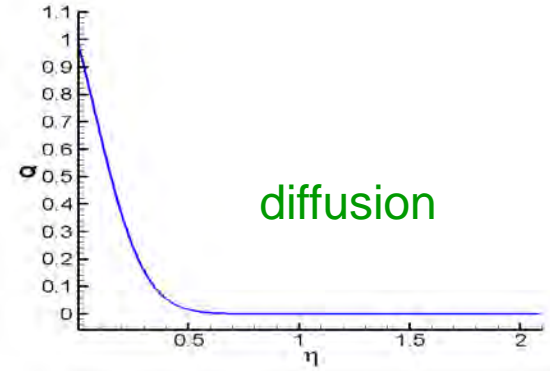
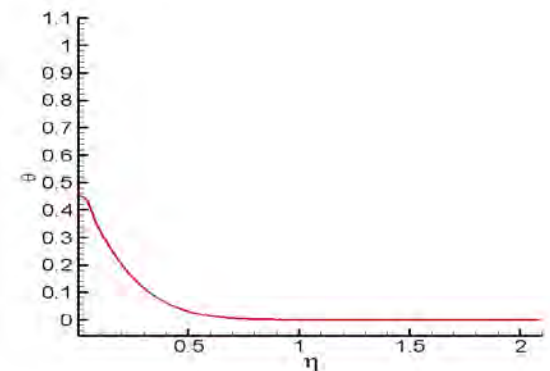
CV model



DPL model



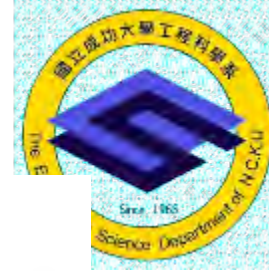
Diffusion



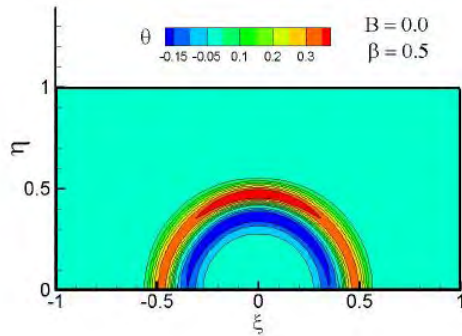
Chou Y and Yang RJ, 2008, *International Journal of Heat and Mass Transfer*, Vol. 51, 3525-3534



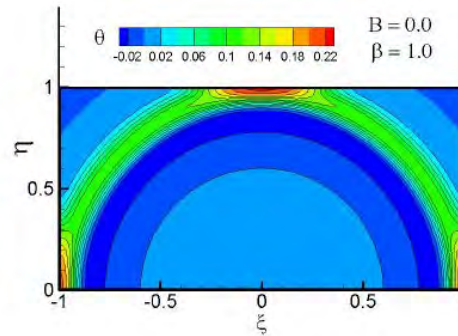
# 2D Thermal Wave



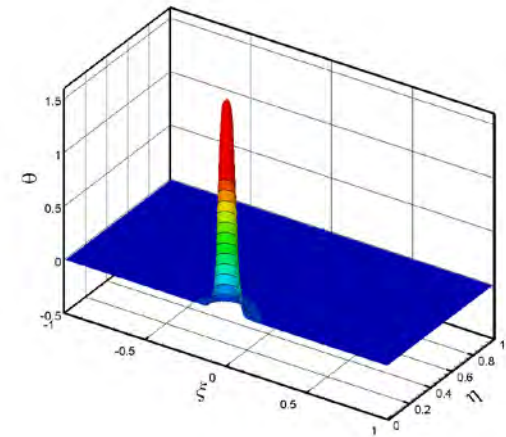
## Wave behavior in the condition of $B=0.0$



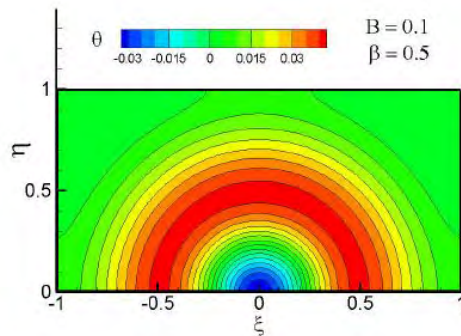
(a)  $\beta = 0.5$



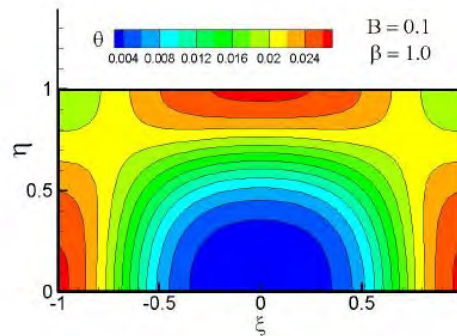
(b)  $\beta = 1.0$



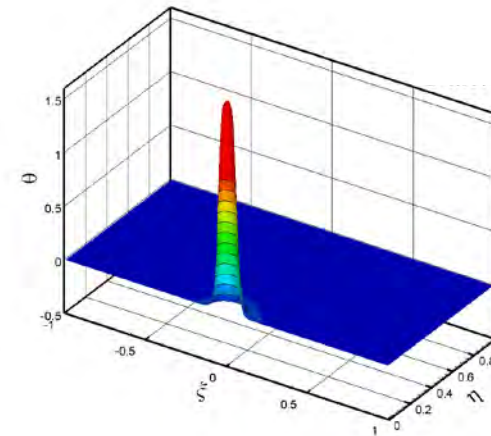
## Wavelike behavior in the condition of $B=0.1$



(a)  $\beta = 0.5$



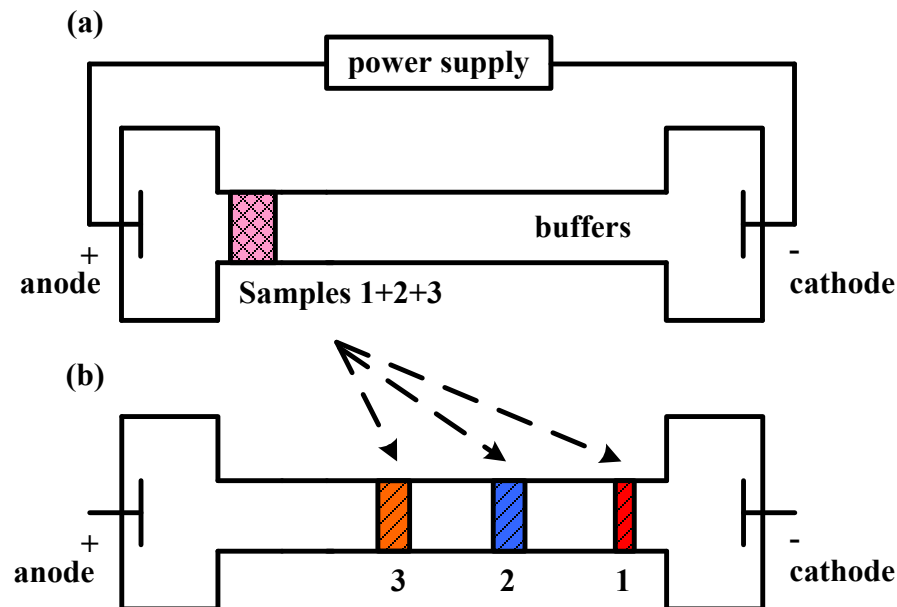
(b)  $\beta = 1.0$



Chou Y and Yang RJ, 2009, *International Journal of Heat and Mass Transfer*, Vol.52, 239-249

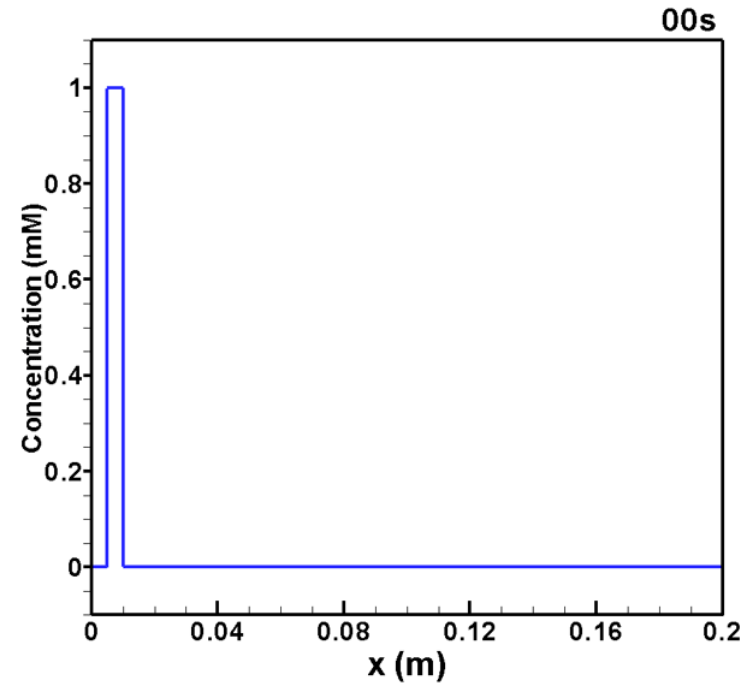
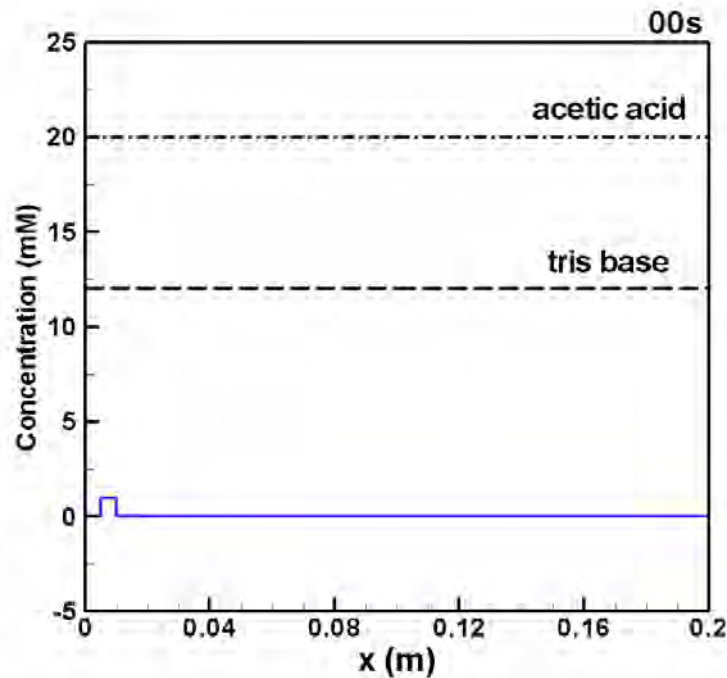
# Zone Electrophoresis

Introduced in the 1960s, the technique of capillary zone electrophoresis (CZE) was designed to separate species based on their size to charge ratio in the interior of a small capillary filled with an electrolyte.



# Validation of CESE scheme in ZE

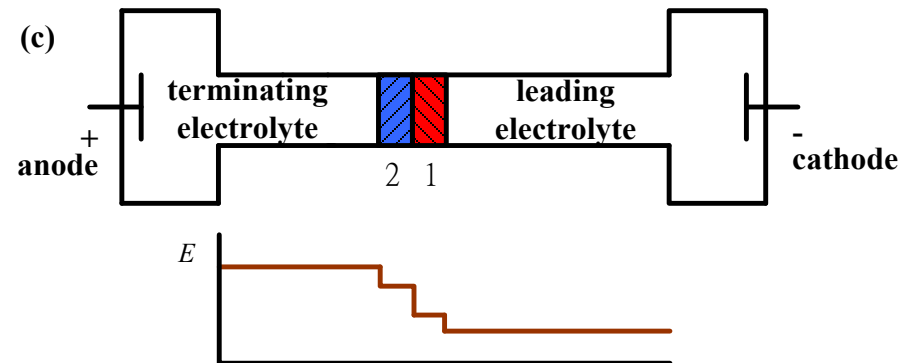
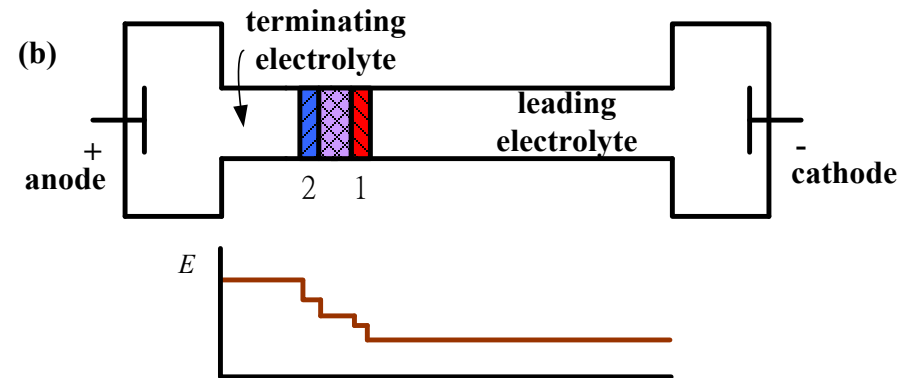
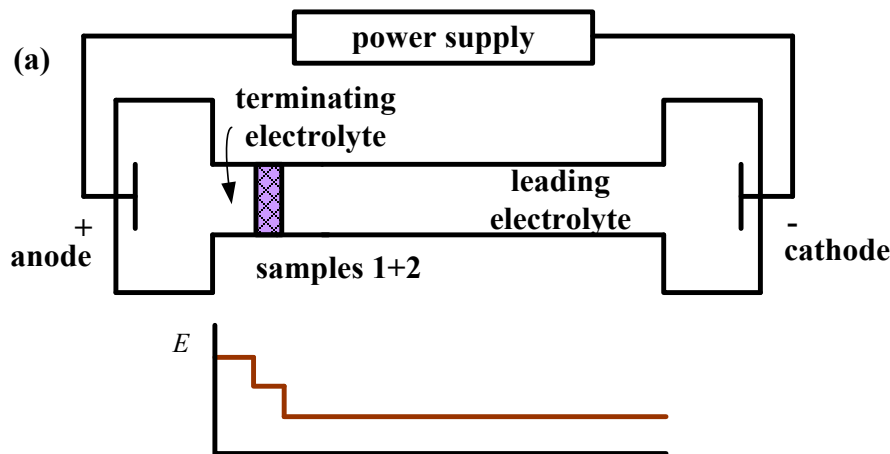
2  $\mu\text{A}$ ,  $\Delta x=25\mu\text{m}$ , 8001 grids



Yu JW, Chou Y and Yang RJ, 2008, *Electrophoresis*, Vol.29, 1048-1057

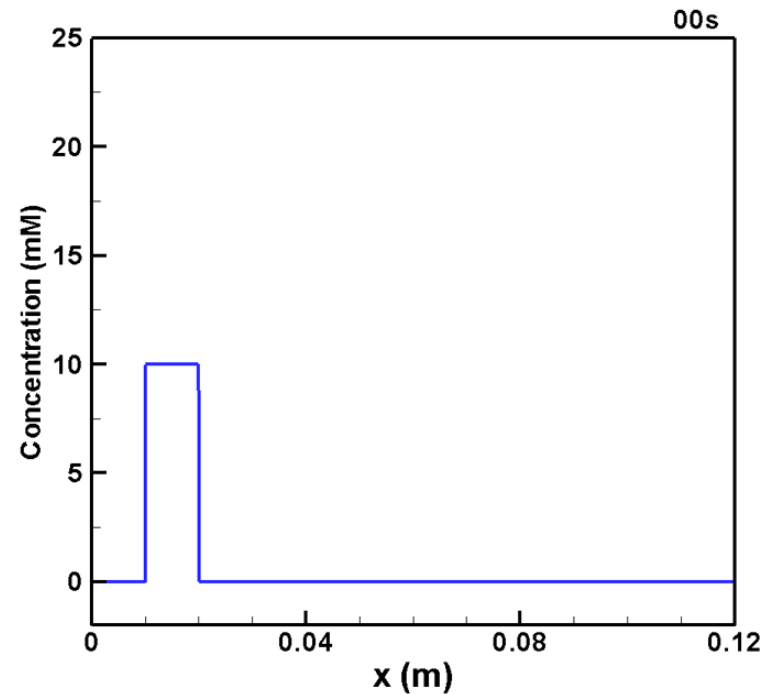
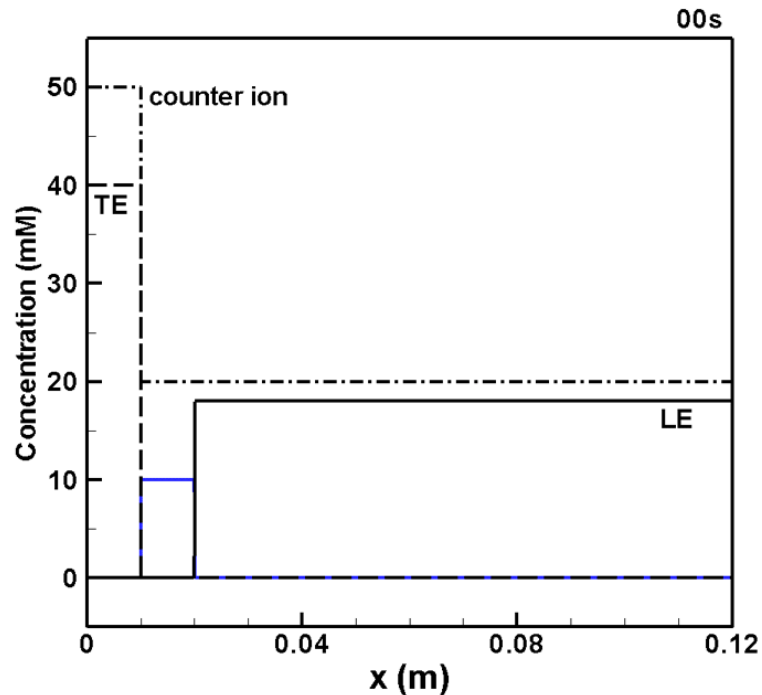
# IsoTachoPhoresis (ITP)

- **Isotachophoresis (ITP)** (Greek: *iso* = equal, *tachos* = speed, *phoresis* = migration) is a technique in analytical chemistry used to separate charged particles.
- In isotachophoresis the sample is introduced between a fast leading electrolyte and a slow terminating electrolyte.



# Validation of CESE scheme in ITP

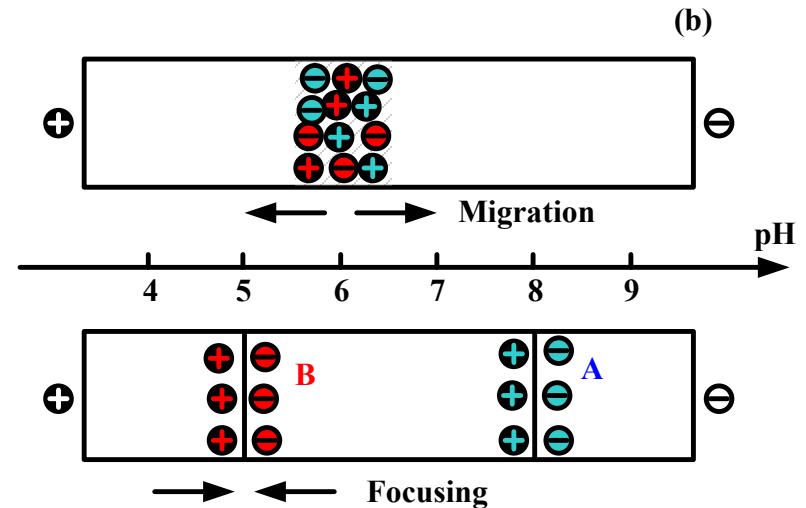
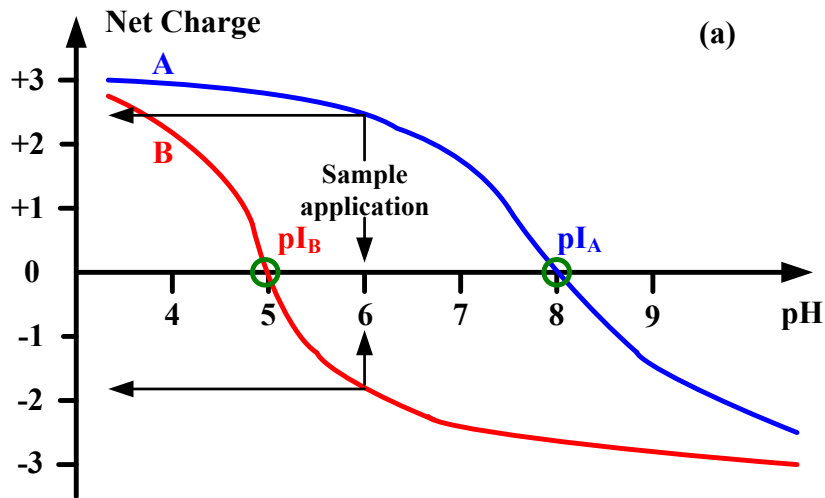
$\Delta x = 100\mu\text{m}$ , 1201 grids



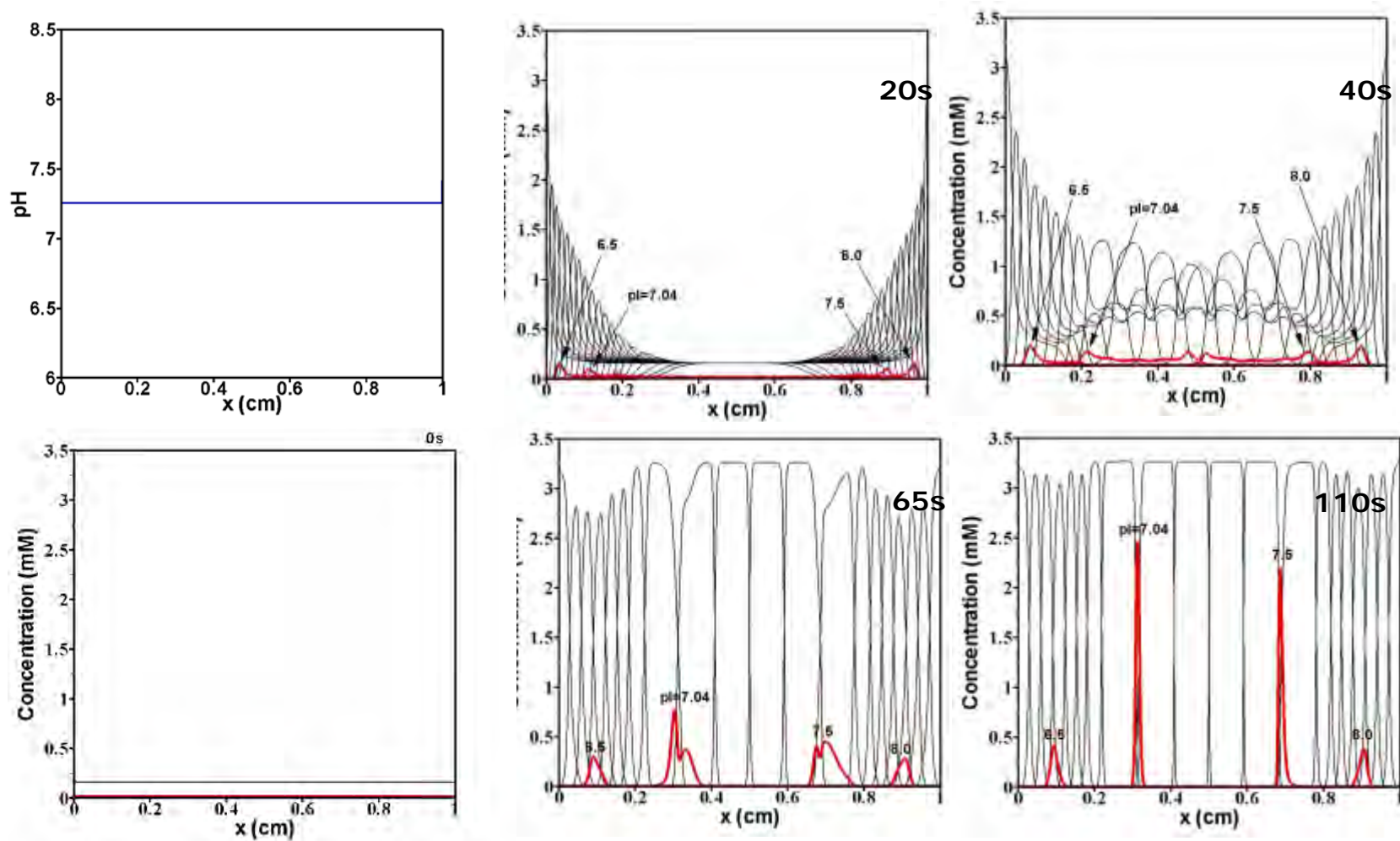
Chou Y and Yang RJ, 2009, *Electrophoresis*, Vol.30, 819-830

# Isoelectric Focusing (IEF)

- The pH at which charge reversal occurs, i.e. where the net charge is zero, is called the isoelectric point, or  $pI$ .



# IEF results- transition solutions



Chou Y and Yang RJ, 2010 *Journal of Chromatography A*, Vol. 1217, 394-404



# *Motivation*

- (1) Applying a fine mesh to solve complex fluid flow problems is computationally expensive.
- (2) Adaptive mesh provides suitable mesh as necessary to save computational cost.
- (3) The solutions in the current time-step are computed directly from the solutions obtained in the previous time-step without the need for extrapolation or interpolation.





# Traditional CESE Method (Stationary Mesh)

Example:  $\frac{\partial u}{\partial t} + a \frac{\partial u}{\partial x} = 0$

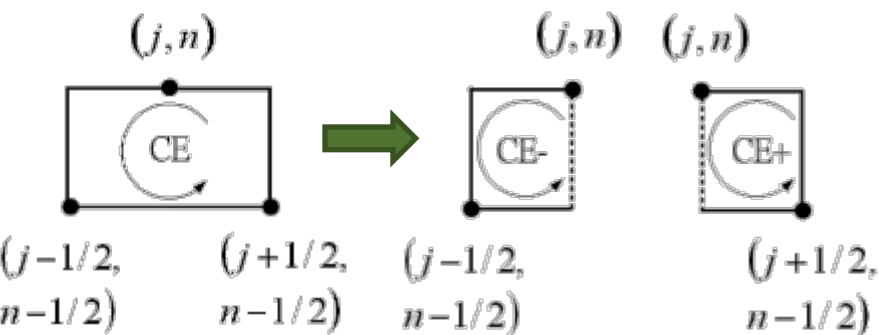
(a is constant speed)

$$\vec{h} = (au, u)$$

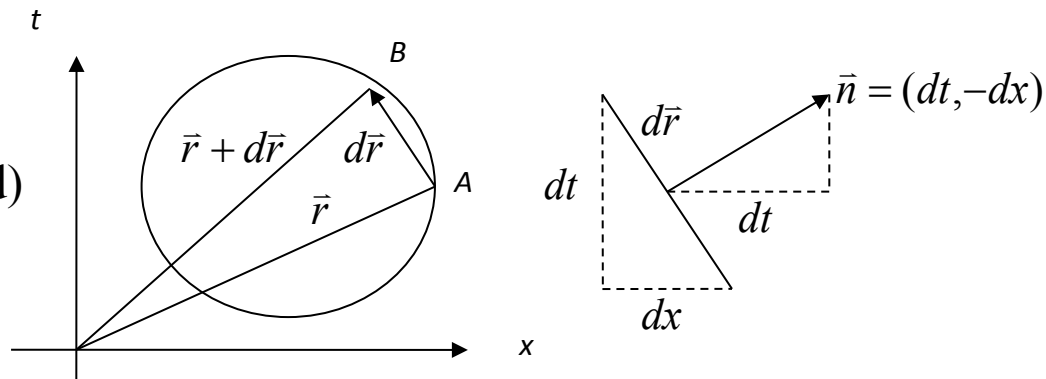
$$\nabla \cdot \vec{h} = \frac{\partial}{\partial x}(au) + \frac{\partial}{\partial t}(u) = 0$$

$$\int_V \nabla \cdot \vec{h} \cdot dV = \int_S \vec{h} \cdot \vec{n} \cdot d\sigma =$$

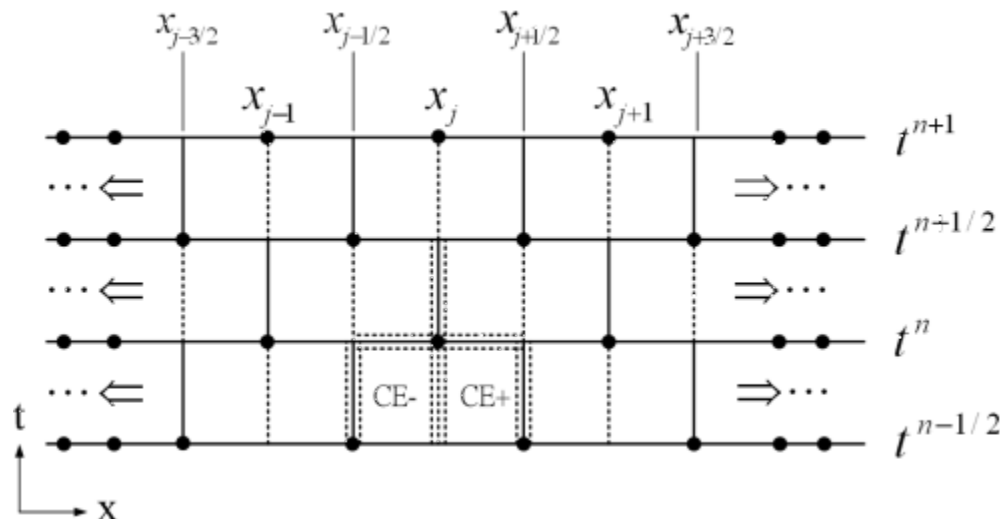
$$\int_S (au, u) \cdot (dt, -dx) = \int_S au \cdot dt - \int_S u \cdot dx = 0$$



Two Eqs.  $\rightarrow$  Solve  $u$  and  $u_x$ .



A surface element  $ds$  and a line segment  $dr$  on the boundary  $S(V)$ .





# ***Introduction of one-dimensional adaptive CESE method***



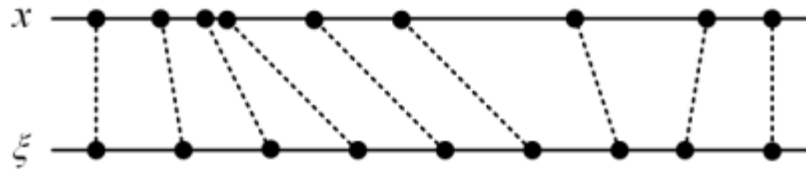
# *Mesh redistribution*

Physical Coordinate:  $\mathbf{x} = (x_1, x_2, \dots, x_d)$

Computational Coordinate:  $\xi = (\xi_1, \xi_2, \dots, \xi_d)$

Quasi-Static Equidistribution Principle

$$(\omega x_\xi)_\xi = 0$$



Monitor Function:  $\omega = \sqrt{1 + \beta(\nabla\Phi)^2}$

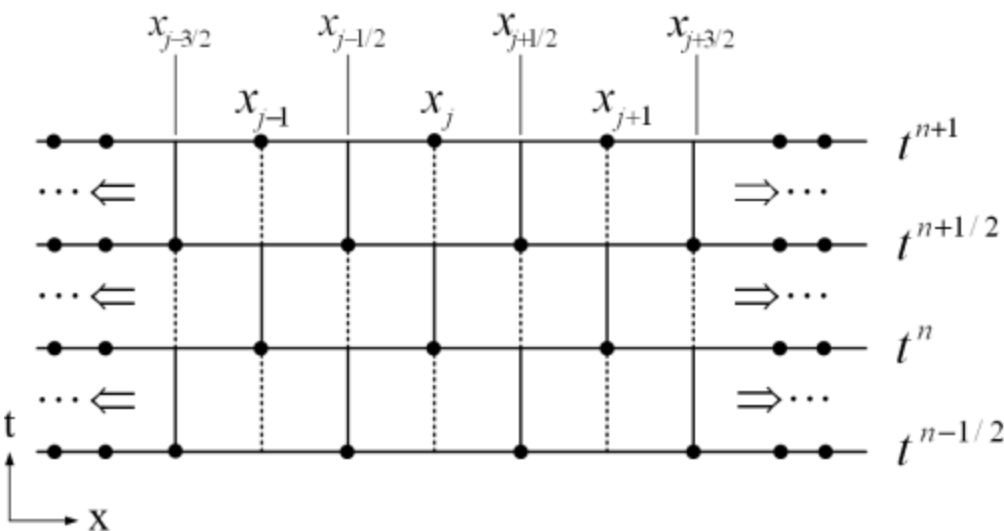
$\Phi$ : Flow variables

$\beta$ : scaling parameter

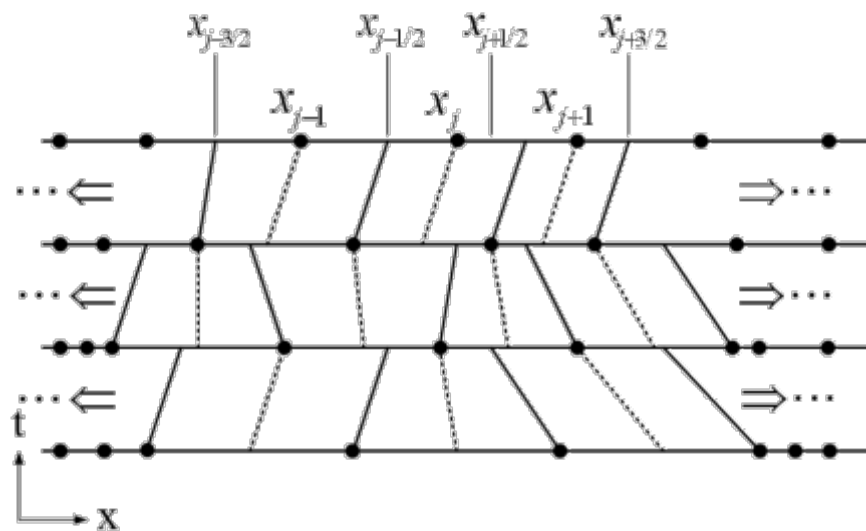


# Space-time domain

Stationary



Moving



The space-time is divided into non-overlapped rectangular regions as the conservation elements and each mesh nodes (marked by filled circle) are setting as the solution elements.



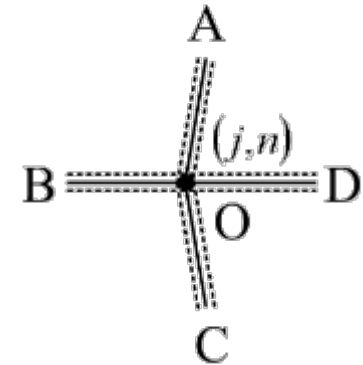
# *The solution element (SE) and conservation element (CE)*

Flow properties are assumed continuous within SE. For any  $(x, y) \in \text{SE}(j, n)$ ,  $u_m(x, t)$  and  $f_m(x, t)$  are approximated by  $u_m^*(x, t)$  and  $f_m^*(x, t)$ .

They are defined as :

$$u_m^*(x, t; j, n) = (u_m)_j^n + (u_{mx})_j^n (x - x_j) + (u_{mt})_j^n (t - t^n)$$

$$f_m^*(x, t; j, n) = (f_m)_j^n + (f_{mx})_j^n (x - x_j) + (f_{mt})_j^n (t - t^n)$$

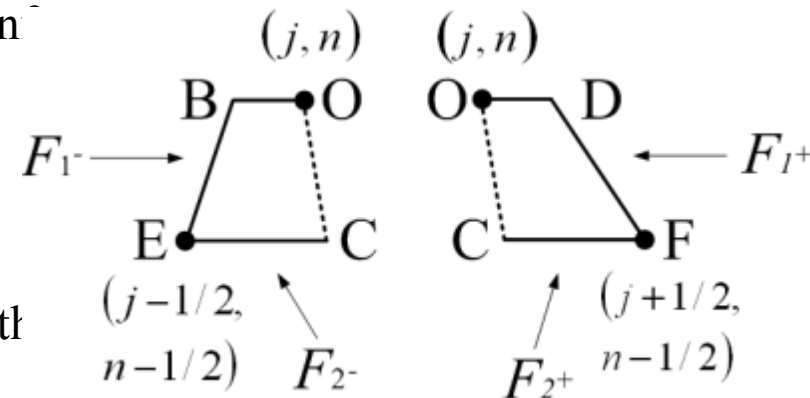


Solution element in point (j,n)

The CE combines two basic CEs, CE+ and CE-, and to enforce flux conservation across CE surfaces we have

$$(u_m)_j^n = -(F_{1-} + F_{2-} + F_{1+} + F_{2+}) / (2\Delta x_3), \quad m = 1, 2, 3$$

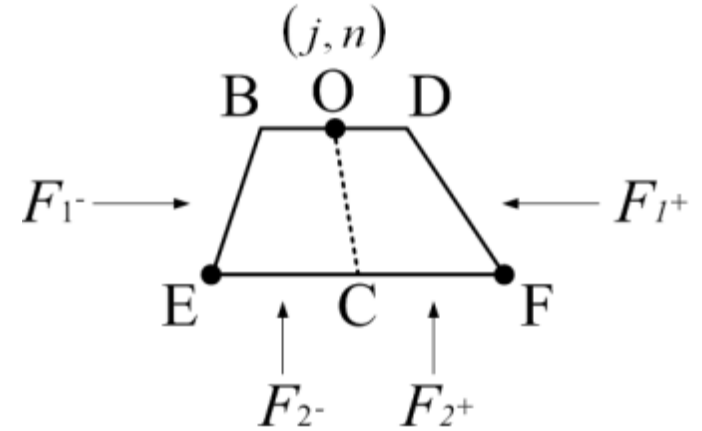
where the  $F_{1-}$ ,  $F_{2-}$ ,  $F_{2+}$  and  $F_{1+}$  denote the fluxes of cross the line segment  $BE$ ,  $EC$ ,  $CF$  and  $FD$ , respectively.



Basic conservation element CE+ and CE-



$$\begin{aligned}
 (1) \quad F_{1^-} &= \oint_{\Gamma(B \rightarrow E)} \mathbf{h}^* \cdot d\mathbf{s} \\
 &= \varphi_m(E) - \varphi_m(B) \\
 &= - \left[ (f_m)_{j-1/2}^{n-1/2} (\Delta t / 2) - (u_m)_{j-1/2}^{n-1/2} (\Delta x_1^-) + (f_{mt})_{j-1/2}^{n-1/2} (\Delta t / 2)^2 / 2 \right. \\
 &\quad \left. - (u_{mx})_{j-1/2}^{n-1/2} (\Delta x_1^-)^2 / 2 + (f_{mx})_{j-1/2}^{n-1/2} (\Delta x_1^-) (\Delta t / 2) \right]
 \end{aligned}$$



$$\begin{aligned}
 (2) \quad F_{2^-} &= \oint_{\Gamma(E \rightarrow C)} \mathbf{h}^* \cdot d\mathbf{s} \\
 &= \varphi_m(C) - \varphi_m(E) \\
 &= - (u_m)_{j-1/2}^{n-1/2} (\Delta x_2^-) - (u_{mx})_{j-1/2}^{n-1/2} (\Delta x_2^-)^2 / 2
 \end{aligned}$$

The compounded conservation elements

$$\begin{aligned}
 (3) \quad F_{2^+} &= \oint_{\Gamma(C \rightarrow F)} \mathbf{h}^* \cdot d\mathbf{s} \\
 &= \varphi_m(F) - \varphi_m(C) \\
 &= - \left[ - (u_m)_{j+1/2}^{n-1/2} (\Delta x_2^+) - (u_{mx})_{j+1/2}^{n-1/2} (\Delta x_2^+)^2 / 2 \right]
 \end{aligned}$$

$$\begin{aligned}
 (4) \quad F_{1^+} &= \oint_{\Gamma(F \rightarrow D)} \mathbf{h}^* \cdot d\mathbf{s} \\
 &= \varphi_m(D) - \varphi_m(F) \\
 &= (f_m)_{j+1/2}^{n-1/2} (\Delta t / 2) - (u_m)_{j+1/2}^{n-1/2} (\Delta x_1^+) + (f_{mt})_{j+1/2}^{n-1/2} (\Delta t / 2)^2 / 2 \\
 &\quad - (u_{mx})_{j+1/2}^{n-1/2} (\Delta x_1^+)^2 / 2 + (f_{mx})_{j+1/2}^{n-1/2} (\Delta x_1^+) (\Delta t / 2)
 \end{aligned}$$



The  $(u'_m)^n_{j\pm 1/2}$  is the first-order Taylor's series approximation of  $u_m$  at  $(j\pm 1/2, n)$ .

$$(u'_m)^n_{j\pm 1/2} = (u_m)^{n-1/2}_{j\pm 1/2} + (u_{mx})^{n-1/2}_{j\pm 1/2} (\Delta x_1^\pm) + (u_{mt})^{n-1/2}_{j\pm 1/2} (\Delta t / 2), \quad m = 1, 2, 3,$$

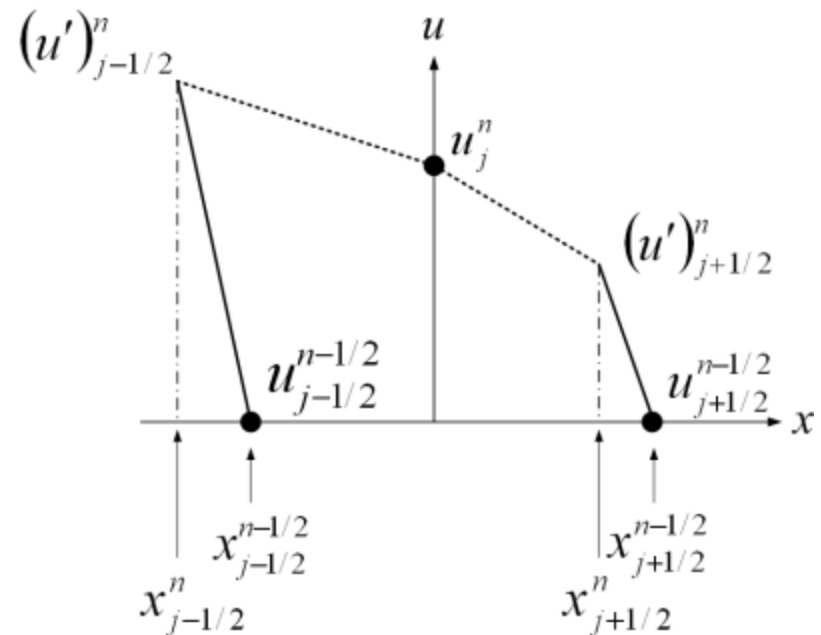
The  $(\hat{u}_{mx^\pm})^n_j$  denote first-order spatial derivatives of the backward and forward differential schemes at point  $(j, n)$ .

$$(\hat{u}_{mx^\pm})^n_j = \frac{(u'_m)^n_{j\pm 1/2} - (u_m)^n_j}{x_{j\pm 1/2}^n - x_j^n}, \quad m = 1, 2, 3$$

The solution gradient  $(\hat{u}_{mx})^n_j$  are evaluated by

$$(\hat{u}_{mx})^n_j = \frac{|\hat{u}_{mx^+}^n_j|^\alpha (\hat{u}_{mx^-}^n_j) + |\hat{u}_{mx^-}^n_j|^\alpha (\hat{u}_{mx^+}^n_j)}{|\hat{u}_{mx^+}^n_j|^\alpha + |\hat{u}_{mx^-}^n_j|^\alpha}$$

$$\left( |\hat{u}_{mx^+}^n_j| + |\hat{u}_{mx^-}^n_j| > 0 \right)$$



Schematic of weighting function



# *Adaptive-CESE Algorithm*

- (1) Give the initial solutions,  $(u_m)_j^0$  and  $(u_{mx})_j^0$  with a uniform mesh to the physical domain at time  $t = 0$ .
- (2) Compute and smooth the monitor function values  $\omega_{j+1/2}$ .
- (3) Move each grid point from its current location  $x_j^\mu$  to a new location  $x_j^{\mu+1}$  using the Gauss-Seidel iteration method.
- (4) Compute the flow variables,  $(u_m)_j^n$  and  $(u_{mx})_j^n$  using the adaptive CESE scheme.
- (5) If  $t^{n+1/2} < T$  output time, set  $(u_m)_j^0 = (u_m)_j^{n+1/2}$  and  $x_j^0 = (x_{j+1/2}^{n+1/2} + x_{j-1/2}^{n+1/2})/2$  and then return to step (2) for the next time step.





# Shock tube problems (1)

(1) The Sod's shock tube problem

$$(\rho, u, p) = \begin{cases} (1.0, 0, 1.0) & \text{if } x \leq 0.5 \\ (0.125, 0, 0.1) & \text{if } x \geq 0.5 \end{cases}$$

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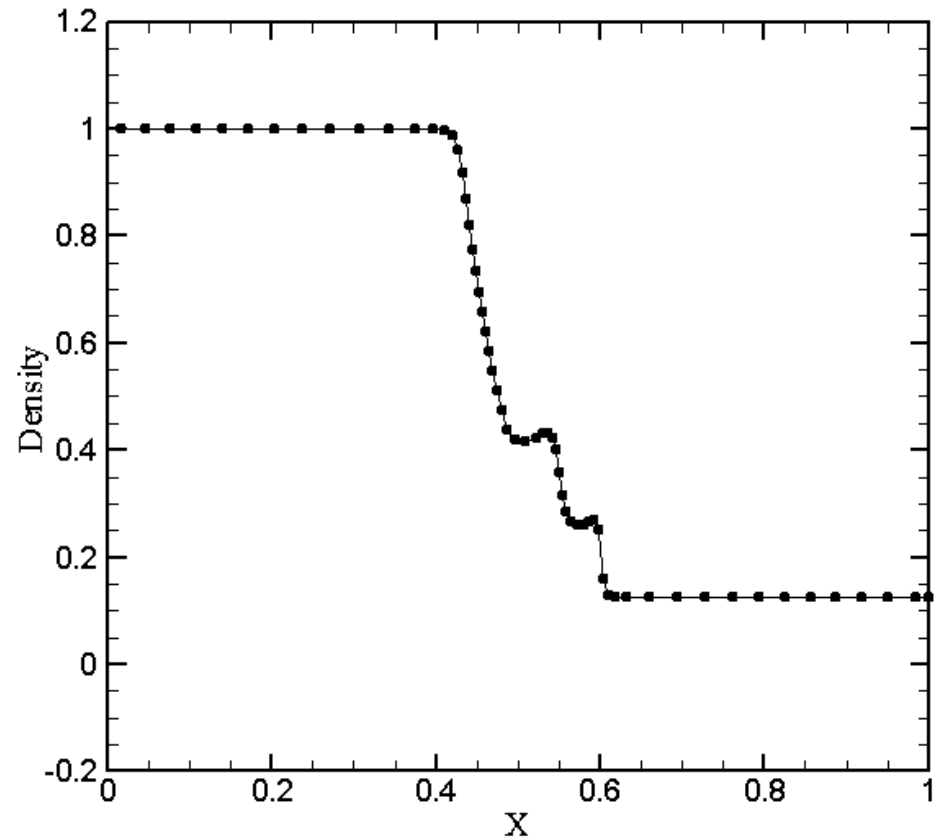
 $\rho_1, u_1, p_1$ 

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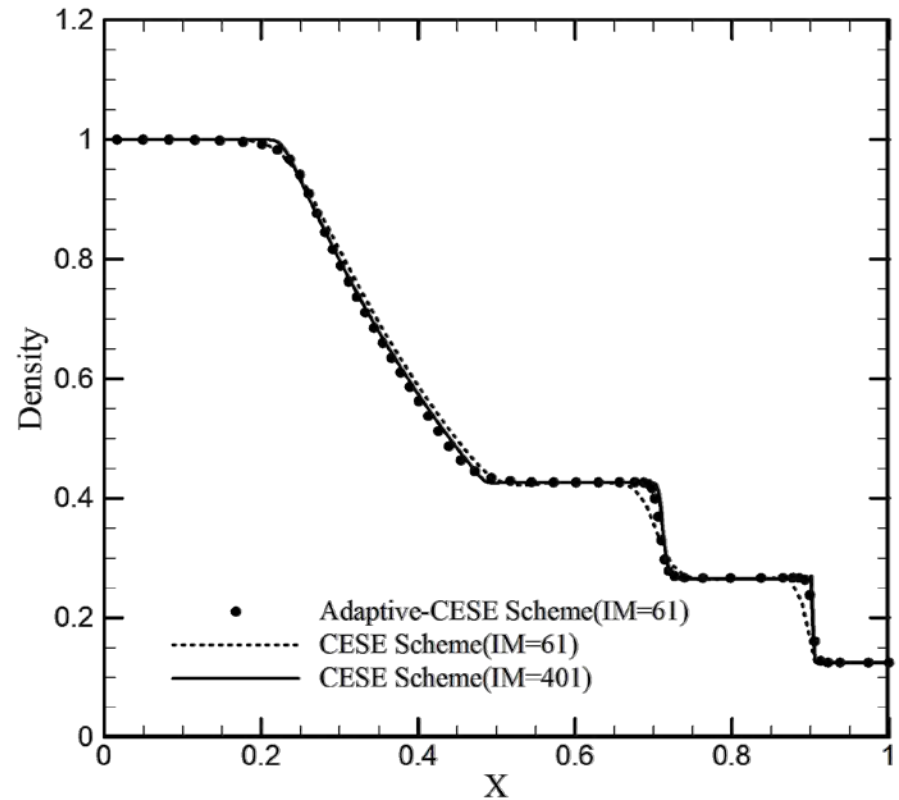
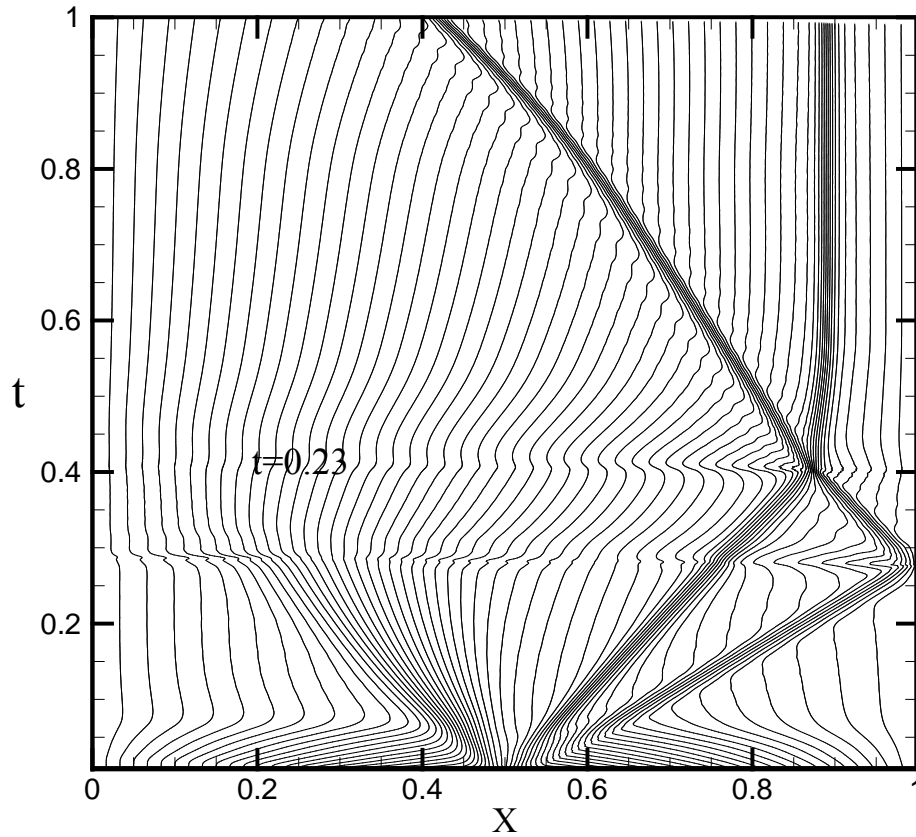
 $\rho_2, u_2, p_2$ 

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# Shock tube problems (1)

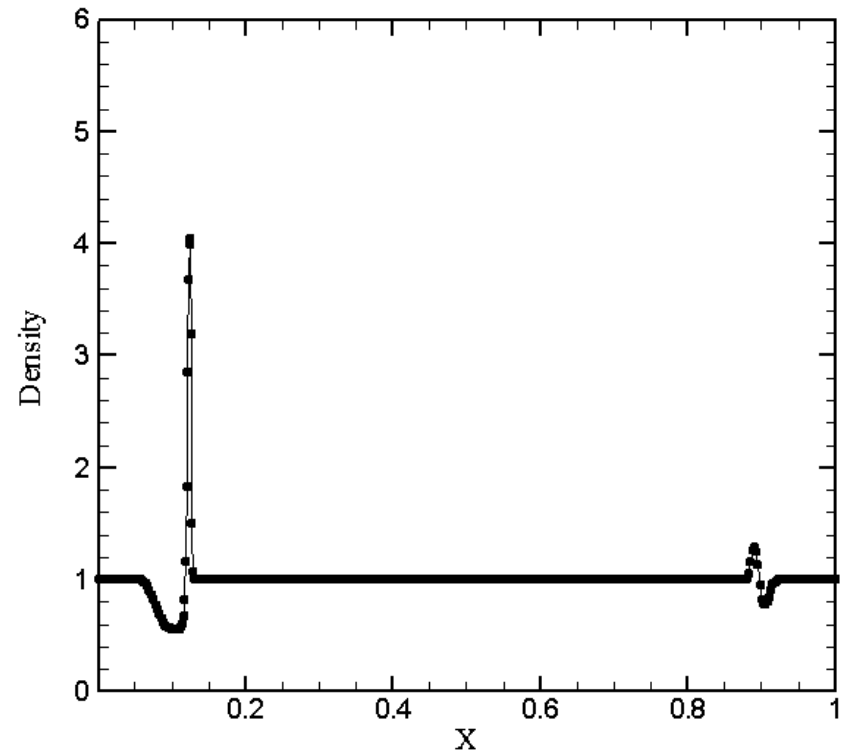
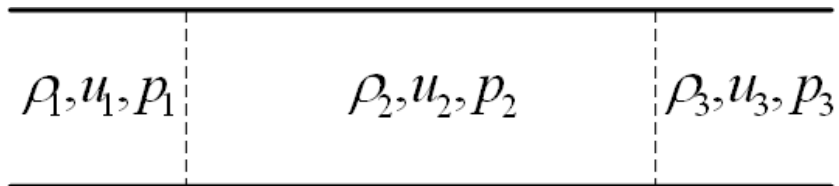




# Shock tube problems (2)

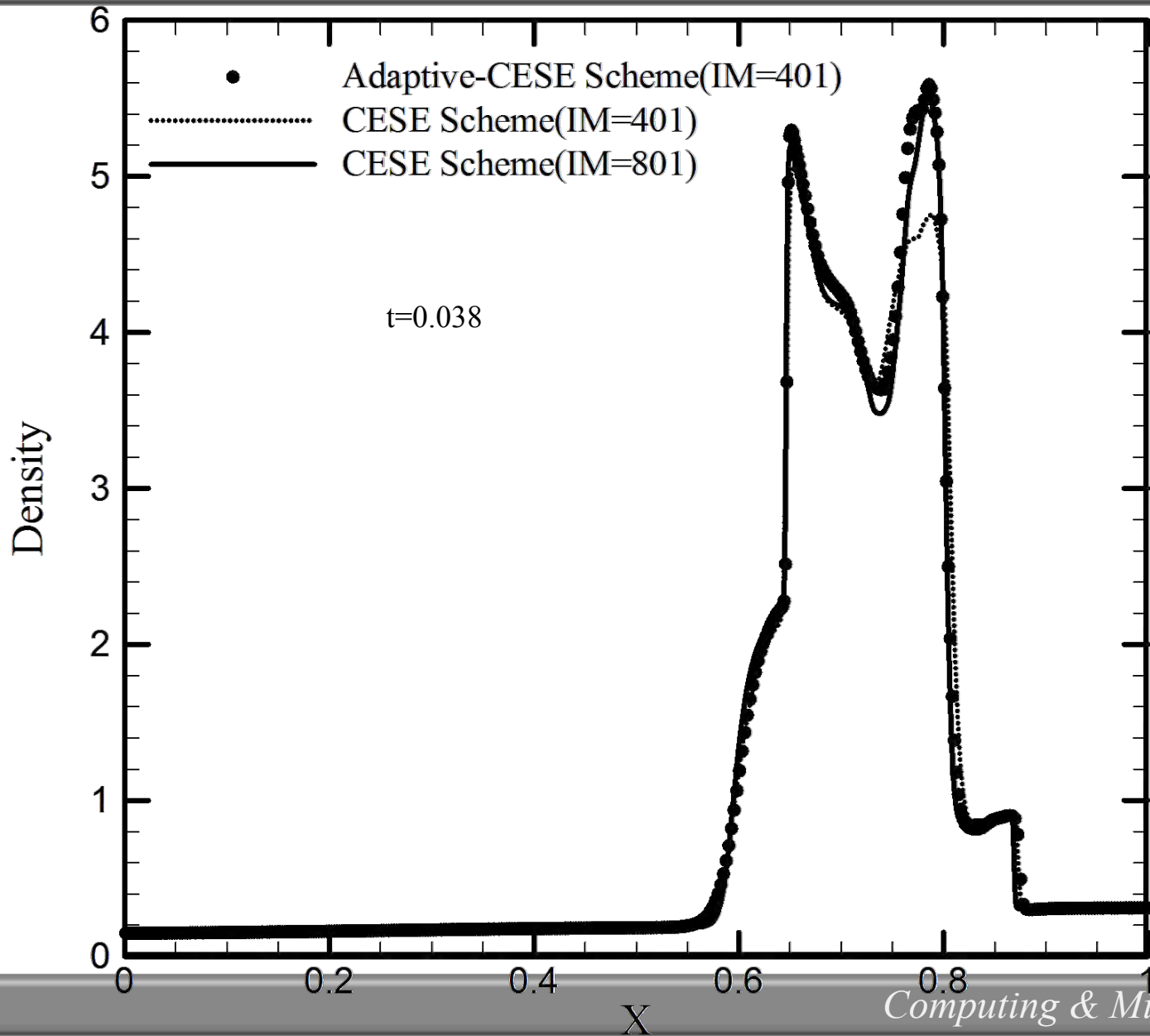
(2) The problem of two interaction blast waves

$$(\rho, u, p) = \begin{cases} (1, 0, 1000) & \text{if } x \leq 0.1 \\ (1, 0, 0.01) & \text{if } 0.1 \leq x \leq 0.9 \\ (1, 0, 100) & \text{if } x \geq 0.9 \end{cases}$$





# *Shock tube problems (2)*

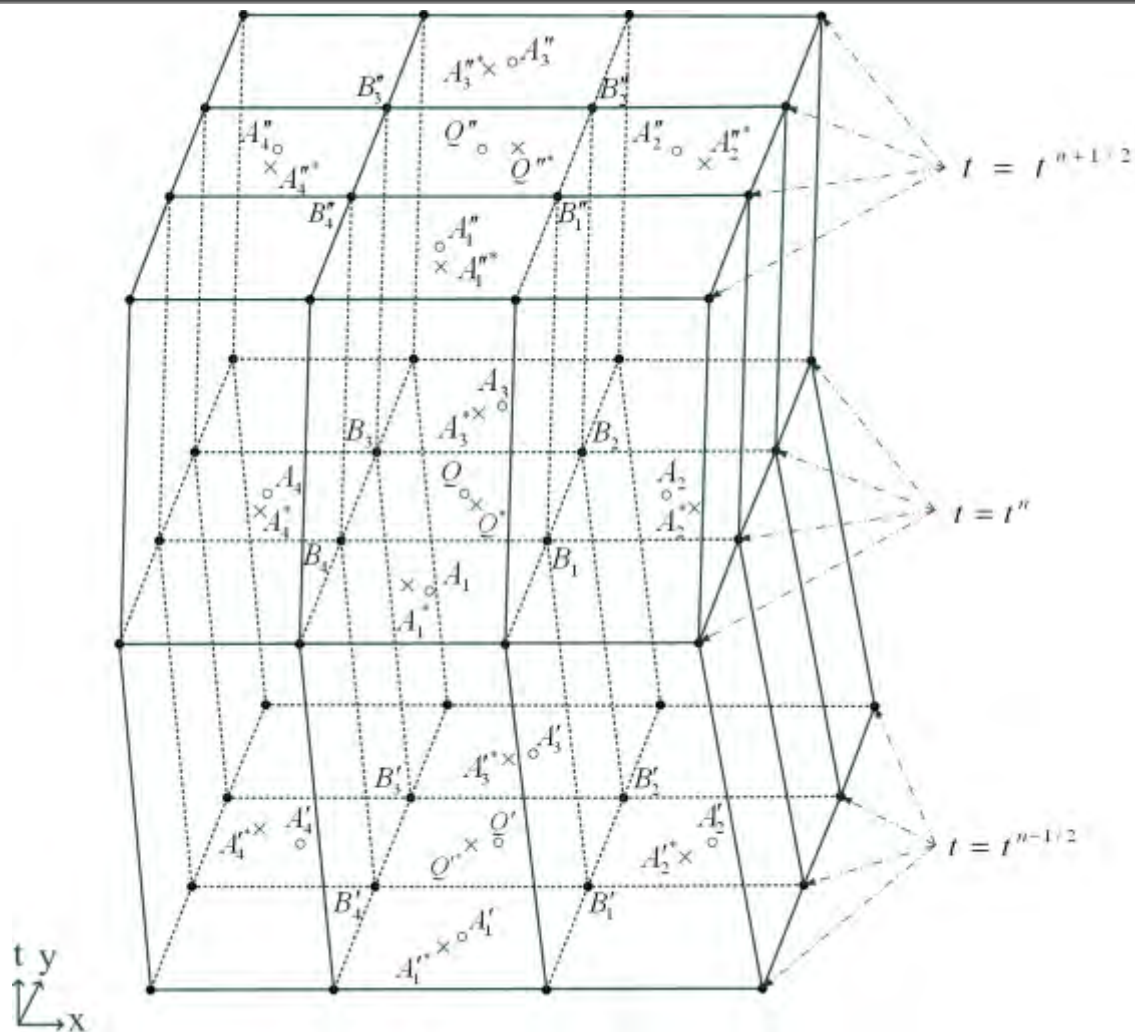




# ***Introduction of two-dimensional adaptive CESE method***



# Space-time domain



The space-time grid points at three adjacent time levels.



# Solution element

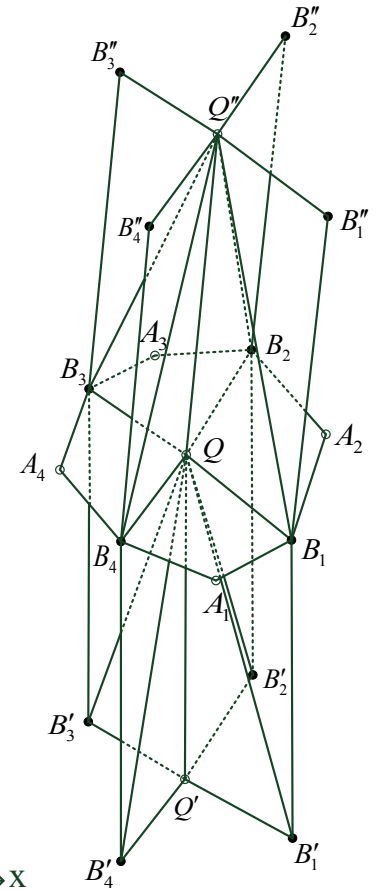
Flow properties are assumed continuities within SE. For any  $(x, y, t) \in SE(Q^*)$  and any  $m = 1, 2, 3, 4$ ,  $u_m(x, y, t)$ ,  $f_m(x, y, t)$ ,  $g_m(x, y, t)$  and  $h_m(x, y, t)$ , respectively, will be approximated by  $u_m^*(x, y, t; Q^*)$ ,  $f_m^*(x, y, t; Q^*)$ ,  $g_m^*(x, y, t; Q^*)$  and  $h_m^*(x, y, t; Q^*)$  to be defined immediately.

Let

$$u_m^*(x, y, t; Q^*) = (u_m)_{Q^*} + (u_{mx})_{Q^*}(x - x_{Q^*}) + (u_{my})_{Q^*}(y - y_{Q^*}) + (u_{mt})_{Q^*}(t - t^n)$$

$$f_m^*(x, y, t; Q^*) = (f_m)_{Q^*} + (f_{mx})_{Q^*}(x - x_{Q^*}) + (f_{my})_{Q^*}(y - y_{Q^*}) + (f_{mt})_{Q^*}(t - t^n)$$

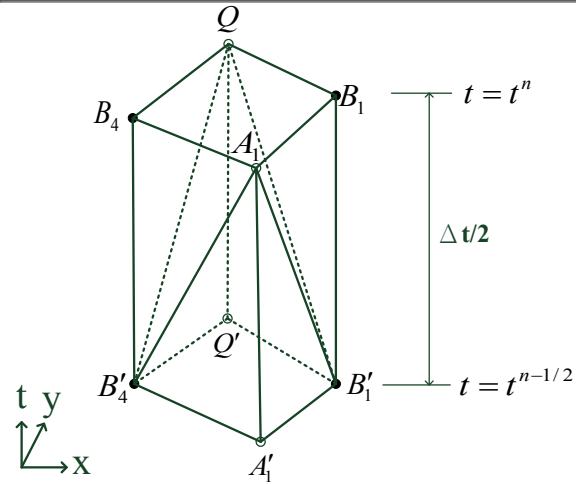
$$g_m^*(x, y, t; Q^*) = (g_m)_{Q^*} + (g_{mx})_{Q^*}(x - x_{Q^*}) + (g_{my})_{Q^*}(y - y_{Q^*}) + (g_{mt})_{Q^*}(t - t^n)$$



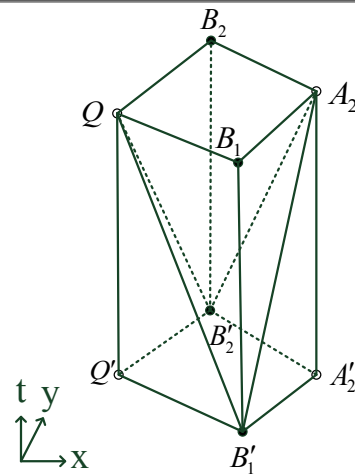
Solution element



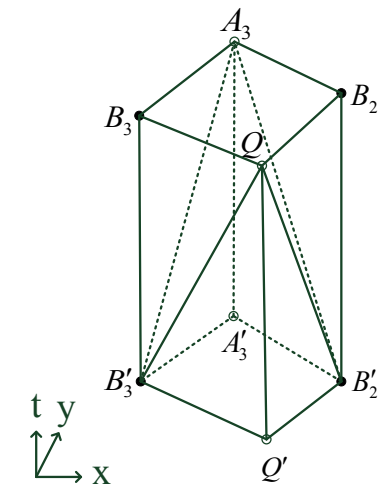
# Basic conservation element



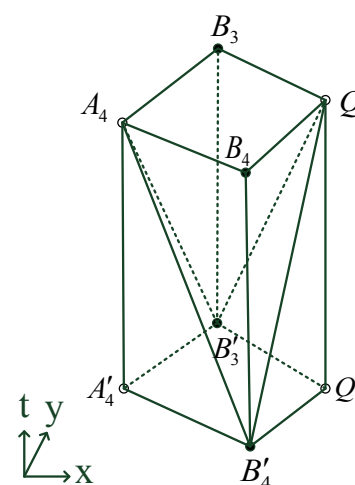
(a)



(b)



(c)



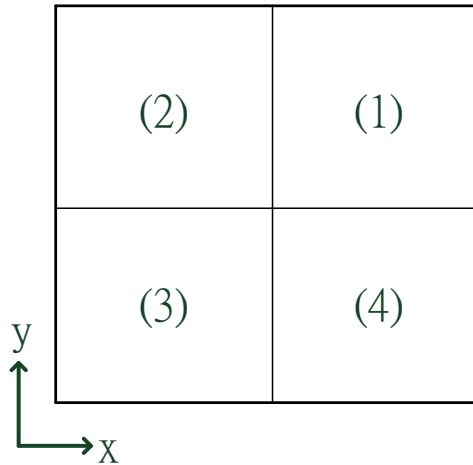
(d)

- (a) The basic conservation element  $CE^{(1)}(Q)$ .
- (b) The basic conservation element  $CE^{(2)}(Q)$ .
- (c) The basic conservation element  $CE^{(3)}(Q)$ .
- (d) The basic conservation element  $CE^{(4)}(Q)$ .





# Two-dimensional Riemann problems



Initial conditions for the two-dimensional Riemann problems.

## Numerical results

- (a) adaptive mesh distribution
- (b) adaptive CESE solution with 150x150 grid points
- (c) the CESE solution with 150x150 grid points.
- (d) the CESE solution with 400x400 grid points.

The spatial computation domain is defined by  $[0,1] \times [0,1]$  and the initial conditions include four constant states.

The four interfaces number are defined as  $(\ell, k) = \{(1, 2), (2, 3), (3, 4), (4, 1)\}$

The forward and backward shock wave is denoted  $S_{\ell k}^+$  and  $S_{\ell k}^-$ .

The forward and backward rarefaction wave is denoted  $R_{\ell k}^+$  and  $R_{\ell k}^-$ .

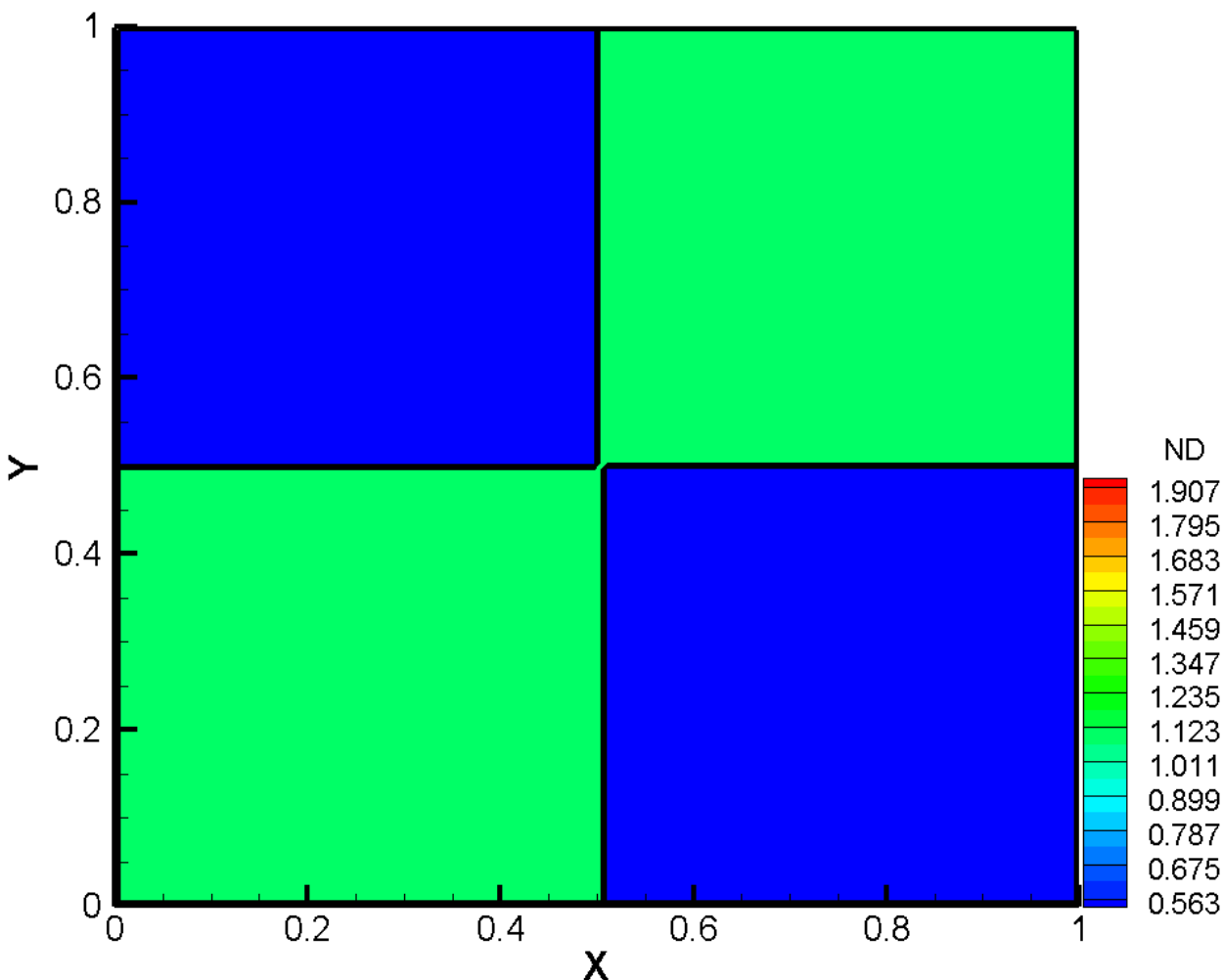
The forward and backward slip line is denoted  $J_{\ell k}^+$  and  $J_{\ell k}^-$ .



# Riemann problems (1)

## Pure shock waves interaction

Sub-case  $S_{12}^+ S_{23}^- S_{34}^+ S_{41}^-$  :

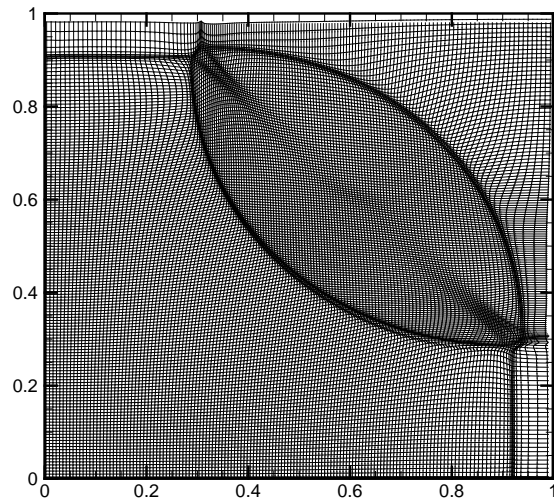


$$(\rho, u, v, p) = \begin{cases} (1.1, 0, 0, 1.1) & \text{----- (1)} \\ (0.5065, 0.8939, 0, 0.35) & \text{-- (2)} \\ (1.1, 0.8939, 0.8939, 1.1) & \text{-- (3)} \\ (0.5065, 0, 0.8939, 0.35) & \text{-- (4)} \end{cases}$$

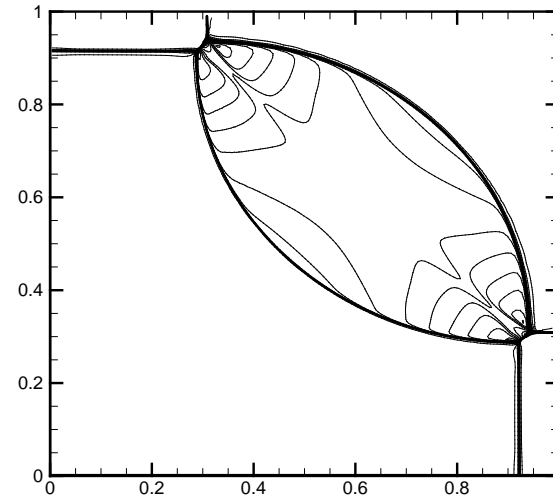


# *Riemann problems (1)*

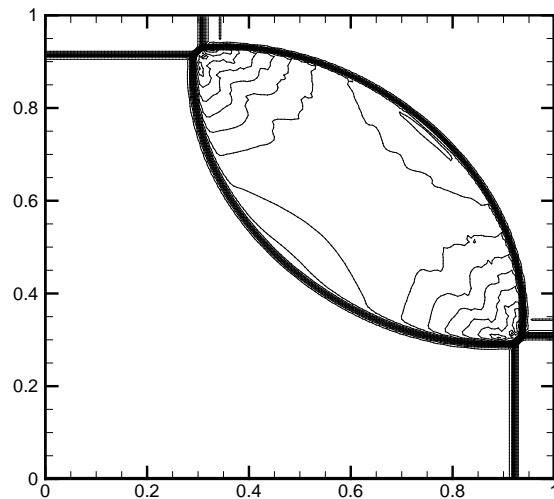
## *Pure shock waves interaction*



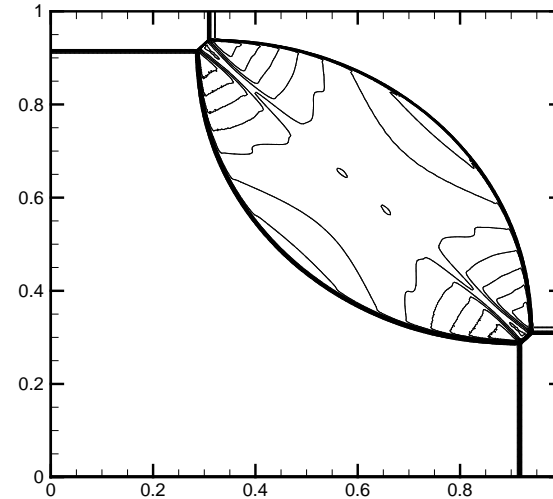
(a)



(b)



(c)



(d)

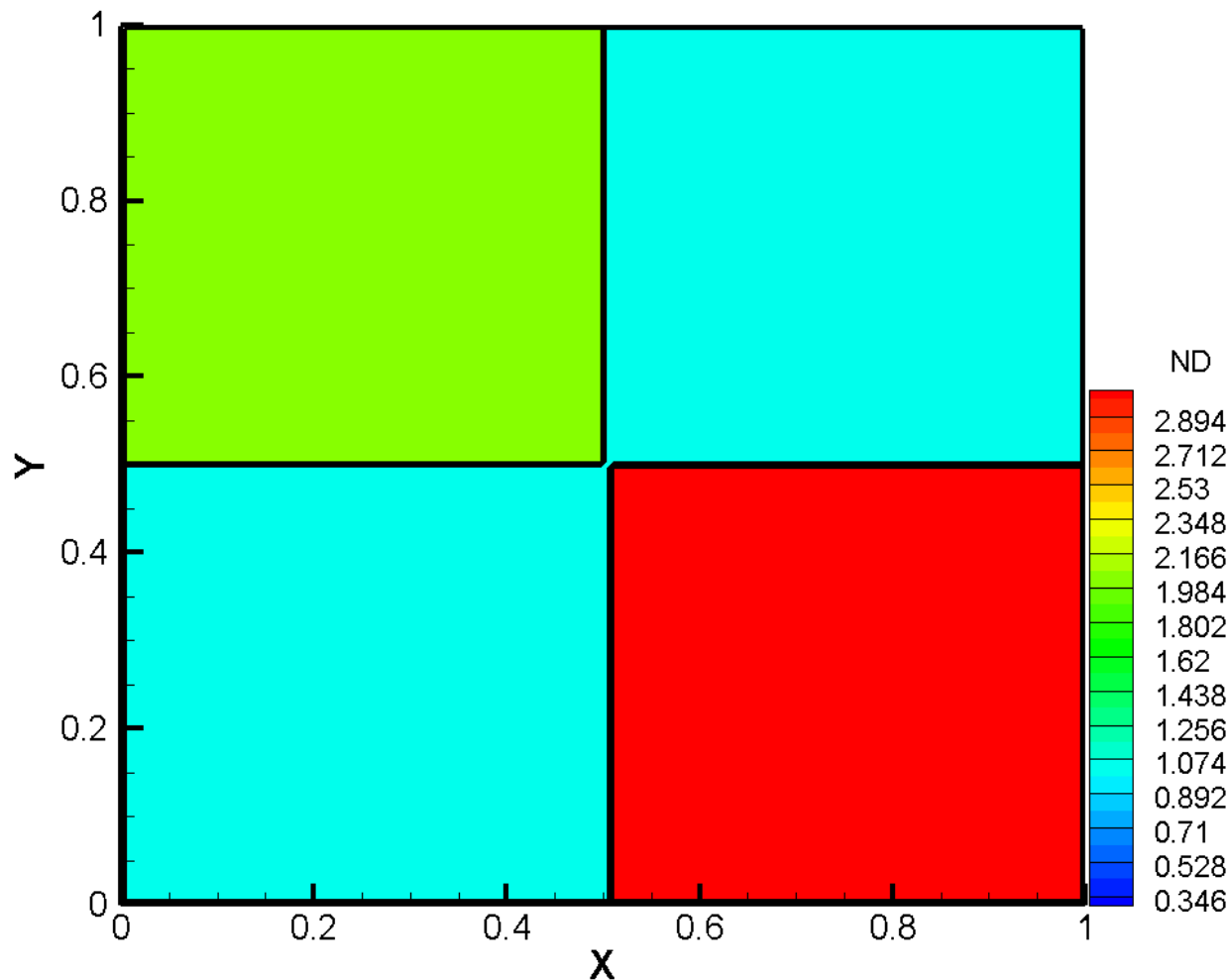


# Riemann problems (2)

## Pure slip line interaction

Sub-case  $J_{12}^- J_{23}^- J_{34}^- J_{41}^- :$

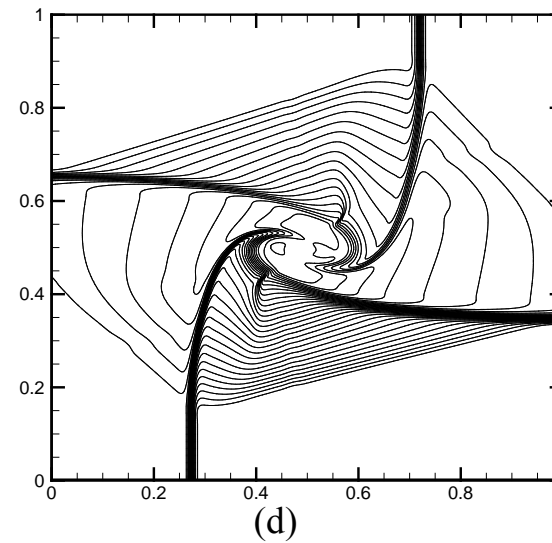
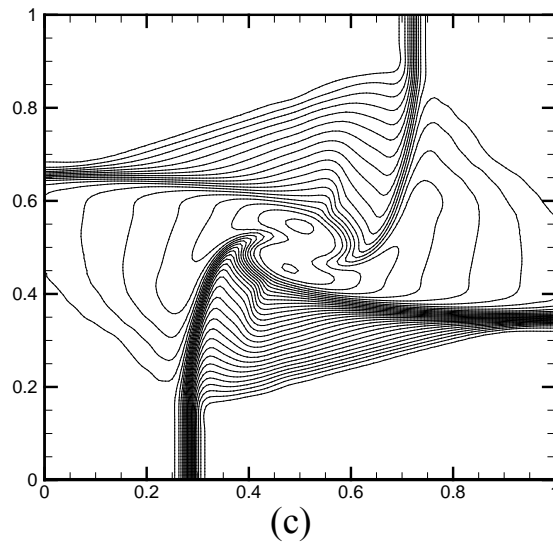
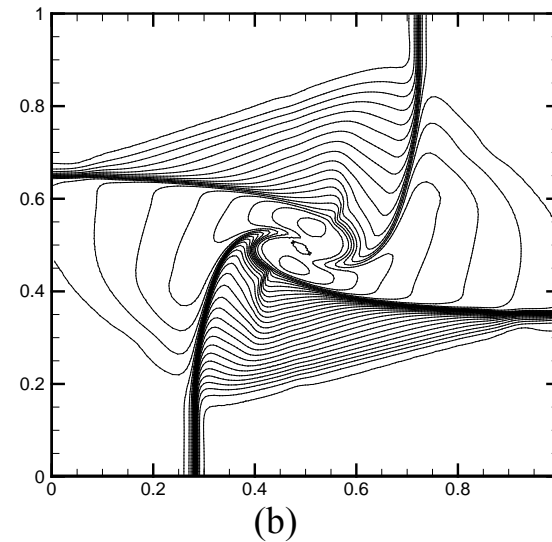
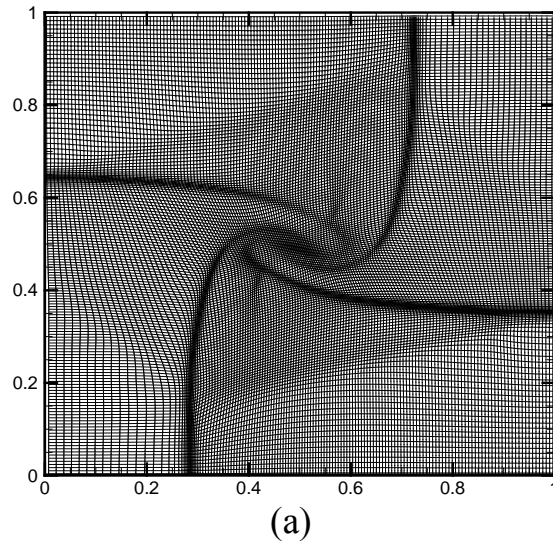
$$(\rho, u, v, p) = \begin{cases} (1, 0.75, -0.5, 1) & \text{--- (1)} \\ (2, 0.75, 0.5, 1) & \text{--- (2)} \\ (1, -0.75, 0.5, 1) & \text{--- (3)} \\ (3, -0.75, -0.5, 1) & \text{-- (4)} \end{cases}$$





# *Riemann problems (2)*

## *Pure slip line interaction*





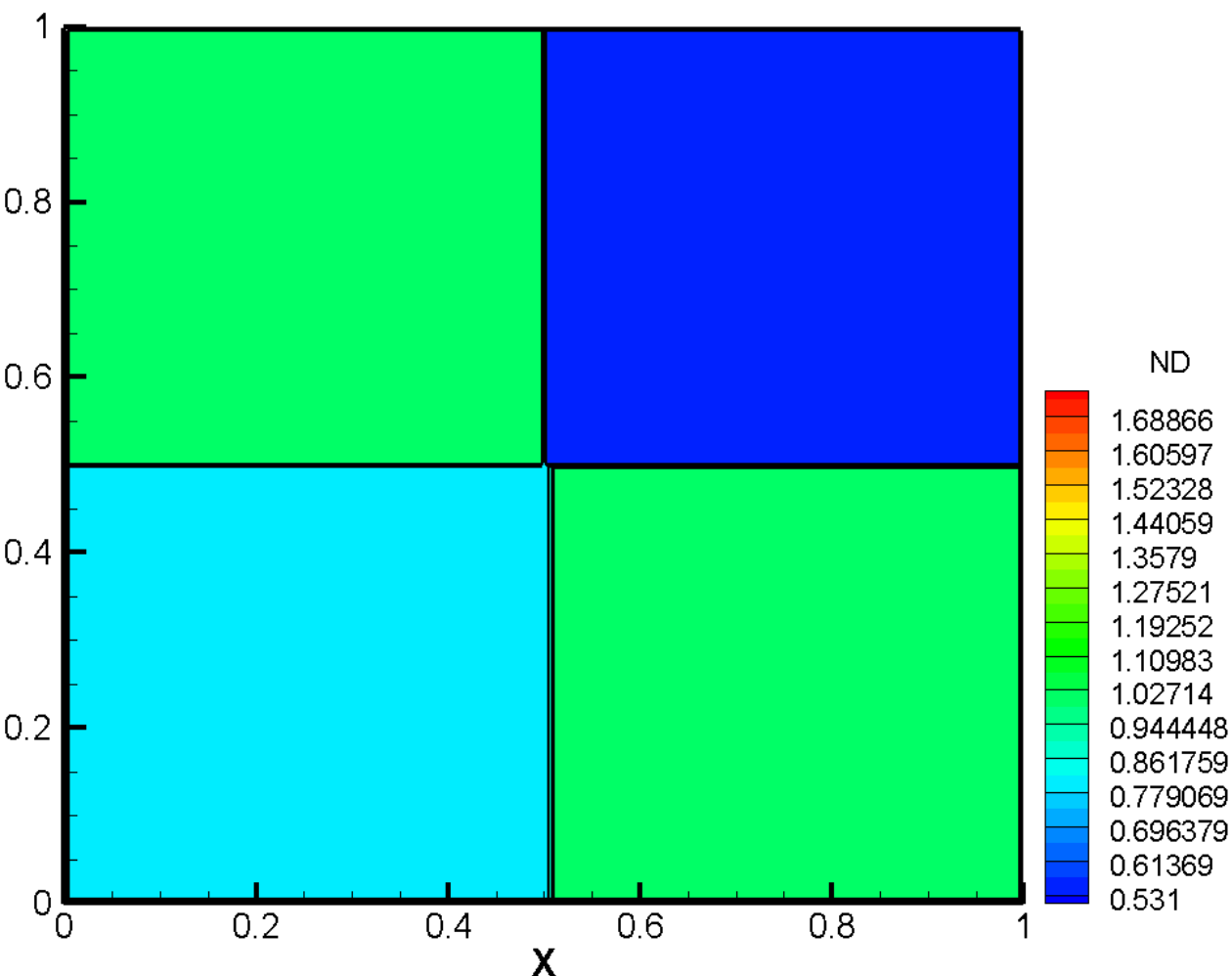
# Riemann problems (3)

## Interaction of multiple waves

Sub-case  $S_{12}^- J_{23}^- J_{34}^+ S_{41}^+$  :

$(\rho, u, v, p) =$

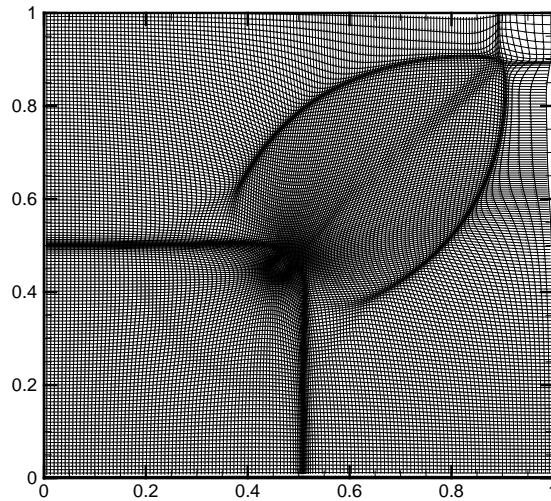
$$\begin{cases} (0.5313, 0, 0, 0.4) \text{ -- (1)} \\ (1, 0.7276, 0, 1) \text{ ---- (2)} \\ (0.8, 0, 0, 1) \text{ ----- (3)} \\ (1, 0, 0.7276, 1) \text{ ---- (4)} \end{cases}$$



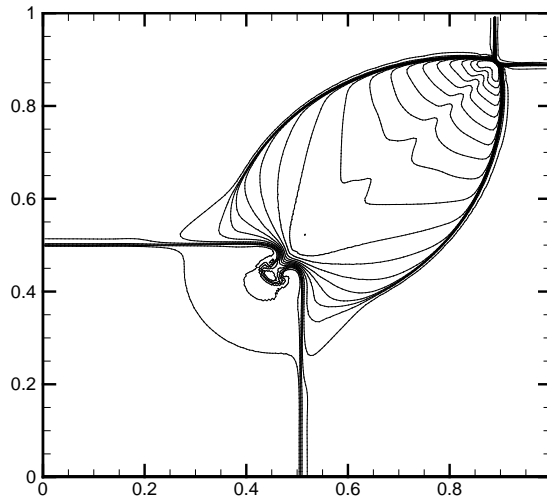


# *Riemann problems (3)*

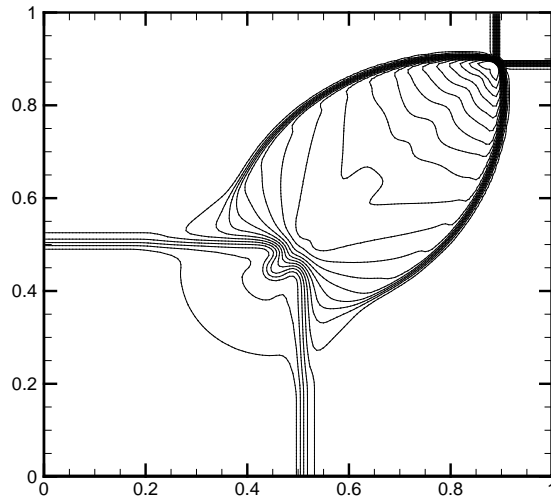
## *Interaction of multiple waves*



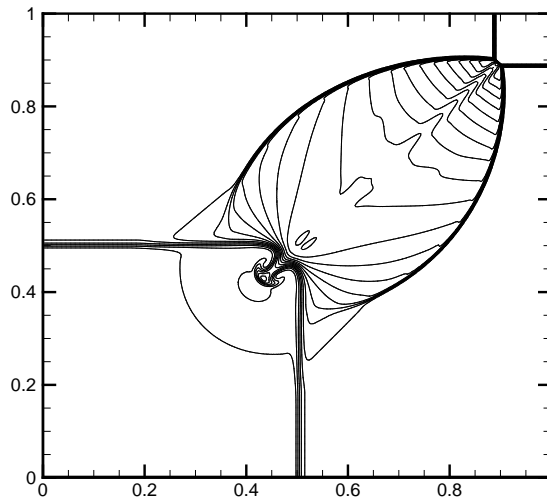
(a)



(b)



(c)



(d)





# *Conclusion*

- (1) The CESE scheme can cover vast range of scales.
- (2) The proposed adaptive CESE scheme in the current time-step is computed directly from the solutions obtained in the previous time-step without the need for extrapolation or interpolation.
- (3) The adaptive CESE scheme captures the flow features with a significantly higher resolution than the original CESE solver.
- (5) The adaptive CESE scheme (implemented on a coarse mesh) achieves the same (or better) resolution as the original stationary CESE solver on a fine mesh, but with a significantly lower computational cost.



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**Progress is impossible without change, and those who  
cannot change their minds cannot change anything.**

*-- George Bernard Shaw, Irish playwright*